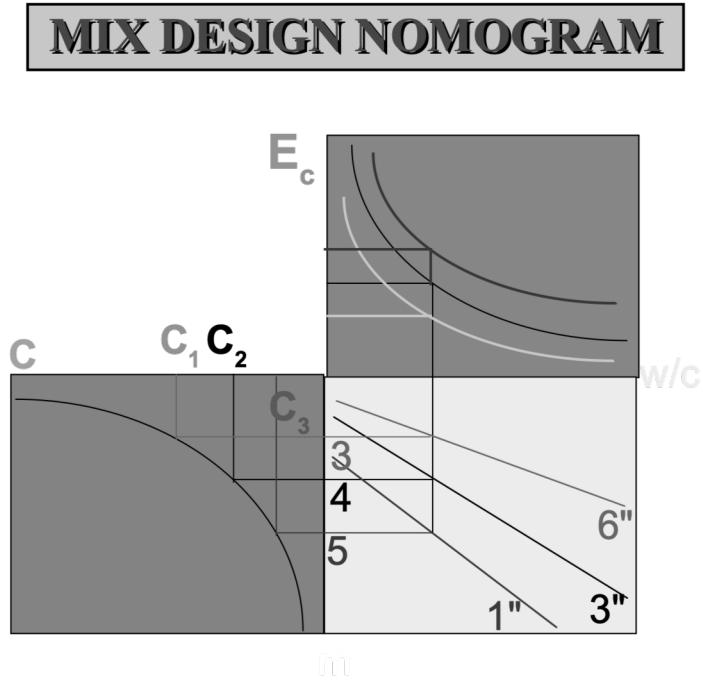


Dosagem do Concreto
Treval Powers

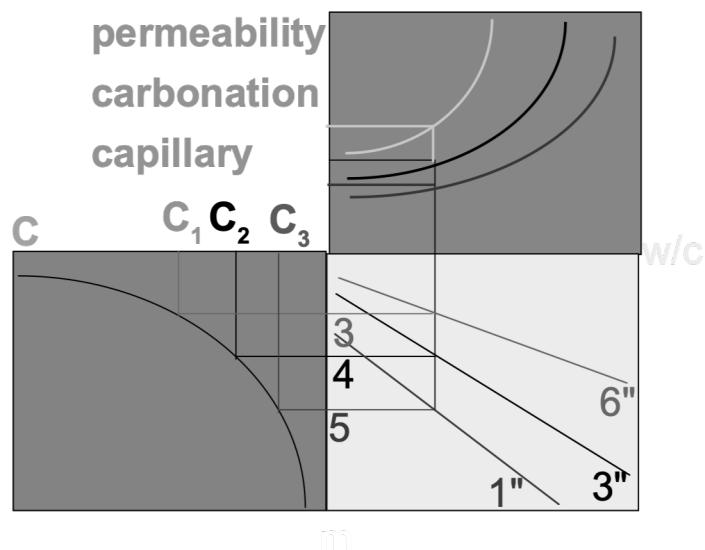
Escola Politécnica
Paulo Helene
20 de agosto de 2009

1



2

MIX DESIGN NOMOGRAM



3

Quais as águas
da pasta hidratada?



4

Química do Cimento Portland

- (100) $\text{C}_3\text{S} + (24) \text{H}_2\text{O} \rightarrow (74) \text{C-S-H} + (49) \text{Ca(OH)}_2$
- (100) $\text{C}_2\text{S} + (21) \text{H}_2\text{O} \rightarrow (100) \text{C-S-H} + (21) \text{Ca(OH)}_2$
- (100) $\text{C}_3\text{A} + (30) \text{H}_2\text{O} \rightarrow$ etringita + aluminato
- (100) $\text{C}_4\text{AF} + (37) \text{H}_2\text{O} \rightarrow$ aluminato + ferrito
- compostos menores

5

água capilar

água de gel

água de
cristalização

6



Qual a água
necessária para
hidratar o cimento?

7

cálculo da água de cristalização:

$$C_3S = 51\% \quad C_2S = 23\% \quad C_fA = 8\%$$

$$C_fAF = 9\% \quad CaO \text{ livre} = 1\% \quad CaSO_4 \cdot 2H_2O = 5\%$$

compostos menores e impurezas = 3 %

$C_3S \rightarrow 51 \cdot 0.24$	$= 12$
$C_2S \rightarrow 23 \cdot 0.21$	$= 4$
$C_fA \rightarrow 8 (0.3 \cdot 1.73 + 0.7 \cdot 0.4)$	$= 6$
$C_fAF \rightarrow 9 \cdot 0.37$	$= 3$

Total $H_2O = 25 \rightarrow 0.25$ da massa cimento

8

$\text{C}_3\text{S} \rightarrow 27.6\% \text{ C-S-H}$; $18.4\% \text{ Ca(OH)}_2$

$\text{C}_2\text{S} \rightarrow 20.8\% \text{ C-S-H}$; $4.3\% \text{ Ca(OH)}_2$

$\text{C}_3\text{A} \rightarrow$ estáveis 3.7% ; instáveis = 5.3%

$\text{C}_4\text{AF} \rightarrow$ estáveis = 10%

total:

• $\text{C-S-H} = 48.8\%$ estáveis = 13.7%

• $\text{Ca(OH)}_2 = 22.7\%$ instáveis = 5.3%

9

...a reação de hidratação se dá com redução de volume equivalente a 25.4% do volume de água que reagiu...

cimento = 1 kg

água de cristalização = 0.25 kg

vol. cimento = $1 / 3.10 = 0.32 \text{ dm}^3$ total

vol. água cristalização = 0.25 dm^3 0.57 dm^3

efetivo —> $0.32 + 0.746 \cdot 0.25 = 0.51 \text{ dm}^3$

10

Powers' Model

gel 100% hidratado

tem 28 % de vazios



para água de
cristalização = 0.26 —>
água de gel = 0.19 da
massa cimento

11

água mínima para
hidratação a 100%

cristalização + gel

$$\rightarrow 0.25 + 0.19 = 0.44$$

12

PRINCIPLES



13

POWERS' MODEL

three water : crystallization, chemical or non-evaporable
gel water (Interlayer + adsorbed)
capillary water (capillary + free)

voids : entrapped air

entrained air

empty pores

capillary water pores

solids products of hydration :

anhydrous cement + chemical water

cement gel ::

solid products + gel water

14

POWERS' MODEL

cement paste :

cement gel + capillary water + air + empty pores

porosity of cement gel : etc (by volume)

gel water / [gel water + solids products] = 27 / 28%

volume of solids products of hydration is less than sum of
volume of anhydrous cement + chemical water :

contraction equivalent 25.6% of reduction

of volume the chemical water

15

POWERS' MODEL

1 : 2 : 3 ; 0.55

type of cement : $C_3S = 50\%$ $C_2S = 22\%$ $C_3A = 13\%$

$C_4AF = 9\%$ others = 6% $\rightarrow w_{ch} = 0.22$

solid products :

by weight : $1 + 0.22 = 1.22$

by volume : $1 / 3.12 + 0.22 / 1.00 = 0.54$ WRONG
 $= 0.32 + 0.22(1 - 0.256) = 0.48$ RIGHT

gel water (from porosity 27%) : $w_{gel} = 0.18$

16

POWERS' MODEL

absolute volume of cement = $1/0.32 = 0.32 \rightarrow 11.6\%$

absolute volume of sand = $2/2.65 = 0.75 \rightarrow 27.1\%$

absolute volume of gravel = $3/2.70 = 1.11 \rightarrow 40.0\%$

absolute volume of water = $0.55/1 = 0.55 \rightarrow 19.8\%$

entrapped air = $1.50\% = 0.04 \rightarrow 1.5\%$

Total volume of concrete = 2.77 $\rightarrow 100\%$

17

1 : 2 : 3 ; 0.55

C = 360 kg/m³ - 600 lb/yd³

FRESH

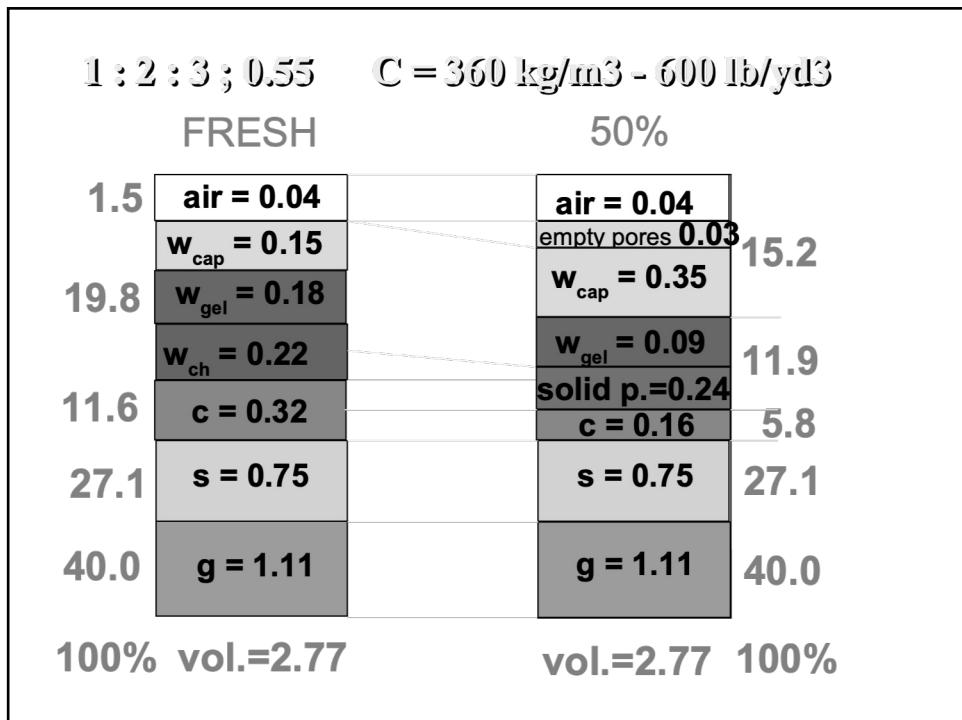
HYDRATED

1.5	air = 0.04		air = 0.04	9.1
	w_{cap} = 0.15		empty pores 0.06	
19.8	w_{gel} = 0.18		w_{cap} = 0.15	23.8
	w_{ch} = 0.22		w_{gel} = 0.18	
11.6	c = 0.32		solid products 0.48	
	s = 0.75		s = 0.75	27.1
27.1	g = 1.11		g = 1.11	40.0

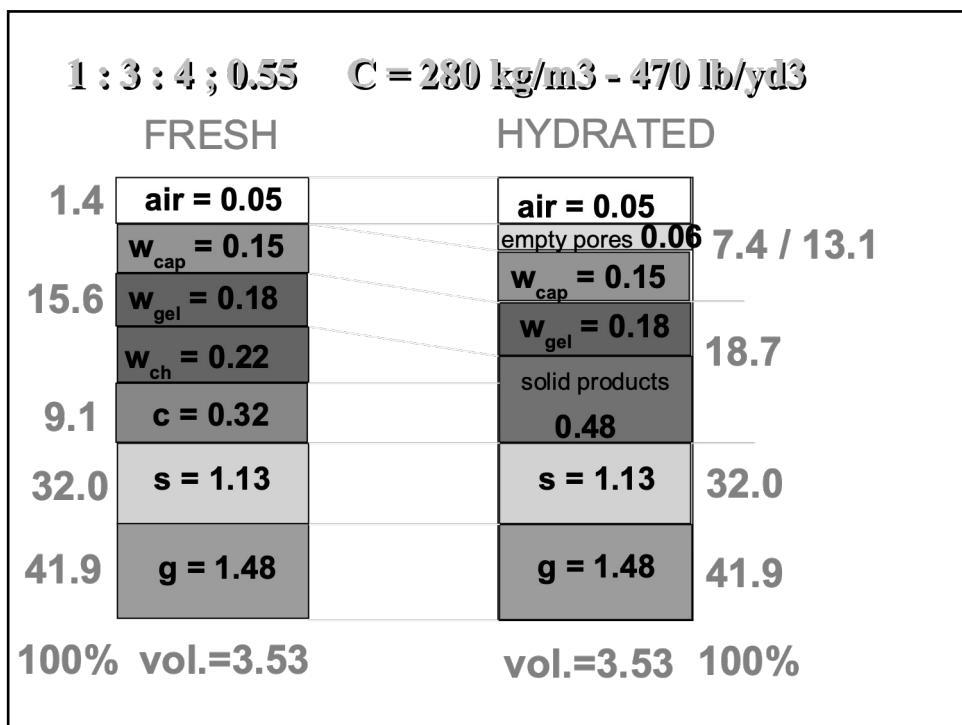
100% vol.=2.77

vol.=2.77 100%

18



19



20

$1 : 1 : 2 ; 0.55 \quad C = 500 \text{ kg/m}^3 - 850 \text{ lb/yd}^3$	
FRESH	HYDRATED
1.0 air = 0.02	air = 0.02
27.4 w_{cap} = 0.15	empty pores 0.06
w_{gel} = 0.18	w_{cap} = 0.15
w_{ch} = 0.22	w_{gel} = 0.18
15.9 c = 0.32	solid products 0.48
18.9 s = 0.38	s = 0.38
36.8 g = 0.74	g = 0.74
100% vol.=2.01	vol.=2.01 100%

21

POWERS' MODEL w/c = cte = 0.55 slump variable				
Mix proportions	Cement content	Aggregate	Cement paste	
(by weight)	(kg/m ³) (lb/yd ³)	s + g	cement gel	voids
1 : 1 : 2	500 / 850	55.7%	32.8%	11.5%
1 : 2 : 3	360 / 600	67.1%	23.8%	9.1%
1 : 3 : 4	280 / 470	73.9%	18.7%	7.4%

How about strength? Permeability? Carbonation? Ions permeability? Creep? Modulus? Drying shrinkage? Durability?

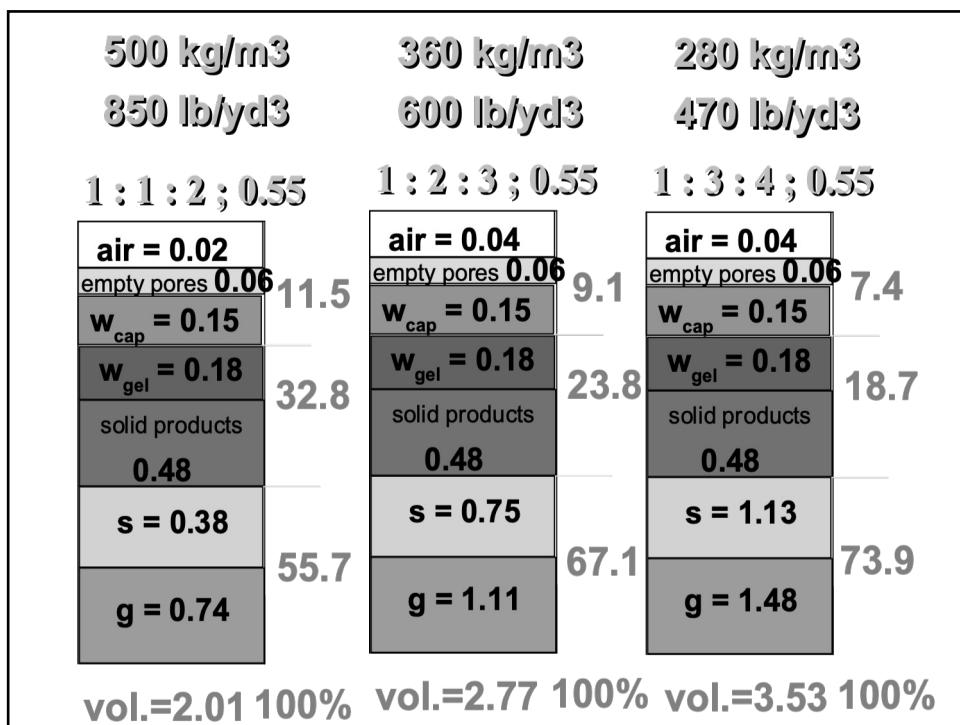
22

POWERS' MODEL w/c variable **slump = cte**

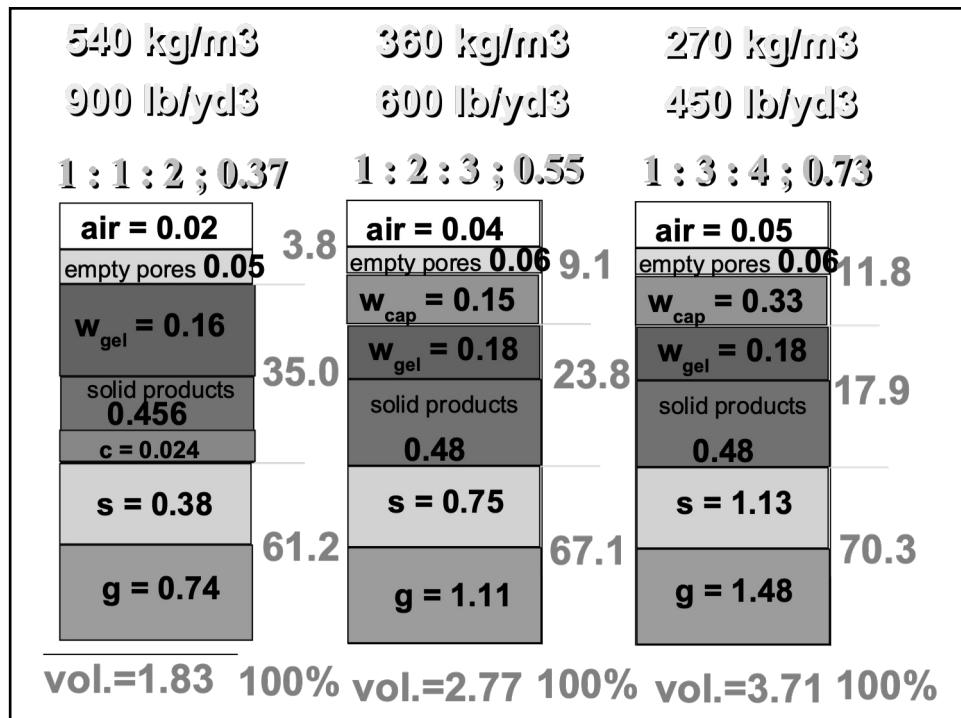
Mix proportions (by weight)	Cement content (kg/m ³) (lb/yd ³)	Aggregate s + g	Cement paste cement ge	voids
1 : 1 : 2 ; 0.37	540 / 900	61.2%	35.0%	3.8%
1 : 2 : 3 ; 0.55	360 / 600	67.1%	23.8%	9.1%
1 : 3 : 4 ; 0.73	270 / 450	70.3%	17.9%	11.8%

How about strength? Permeability?
Carbonation? Ions permeability? Creep?
Modulus? Drying shrinkage? Durability?

23



24



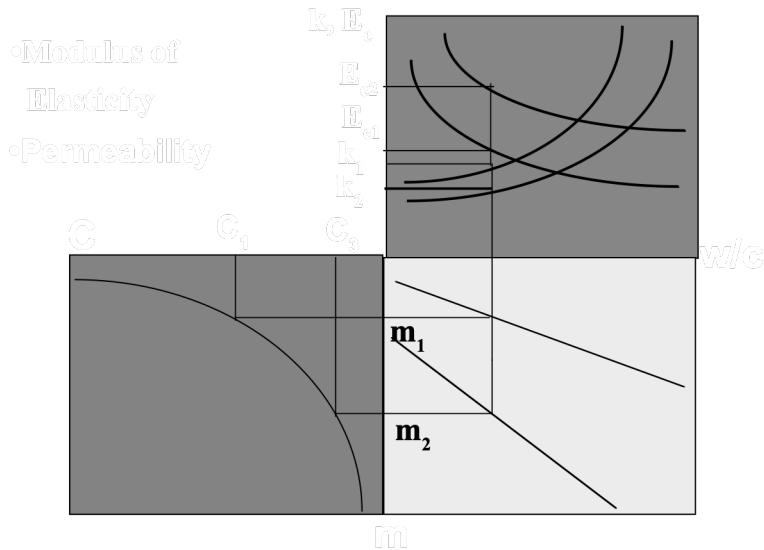
25

HISTORY

- 1824 -> Joseph Aspdin
- 1896 -> Férèt
 $f_c = K [c / (c+w+air)]^2$ (volume)
- 1918 -> Duff Abrams
 $f_c = K_1 / K_2^{w/c}$ (volume)
 *fineness modulus
 *slump test

26

MIX DESIGN NOMOGRAM



27

$w / c = \text{cte}$

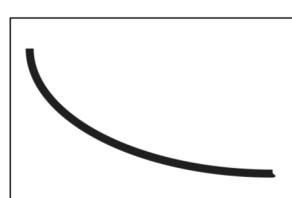
c



aggregates

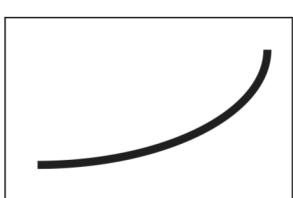
$w / c = \text{variable}$

f_c



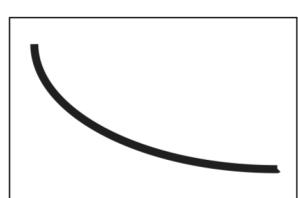
aggregates

E_c



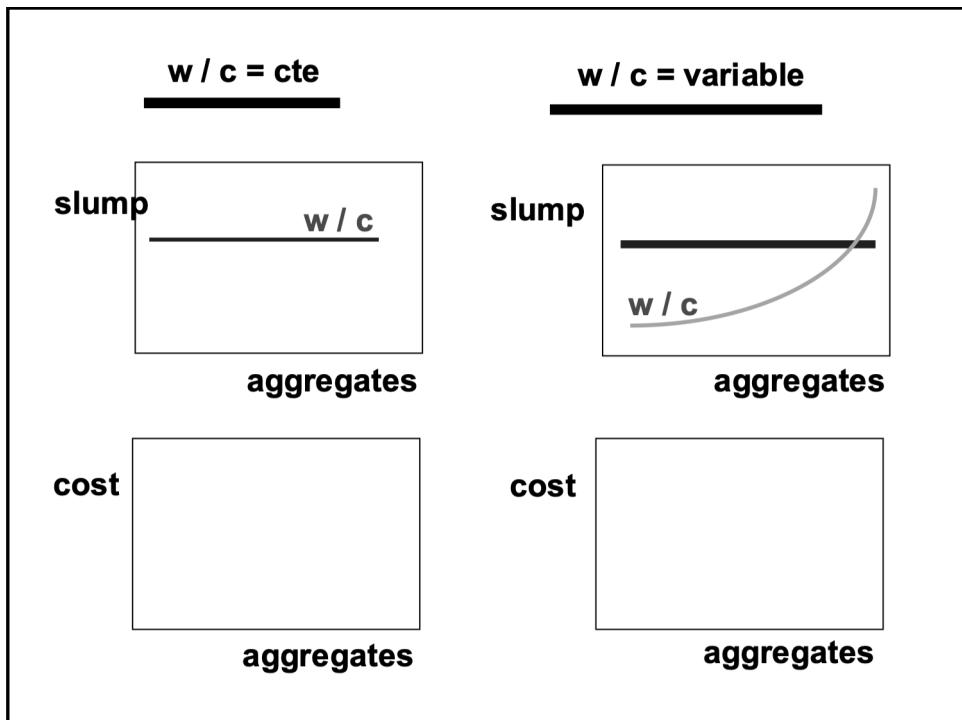
aggregates

E_c

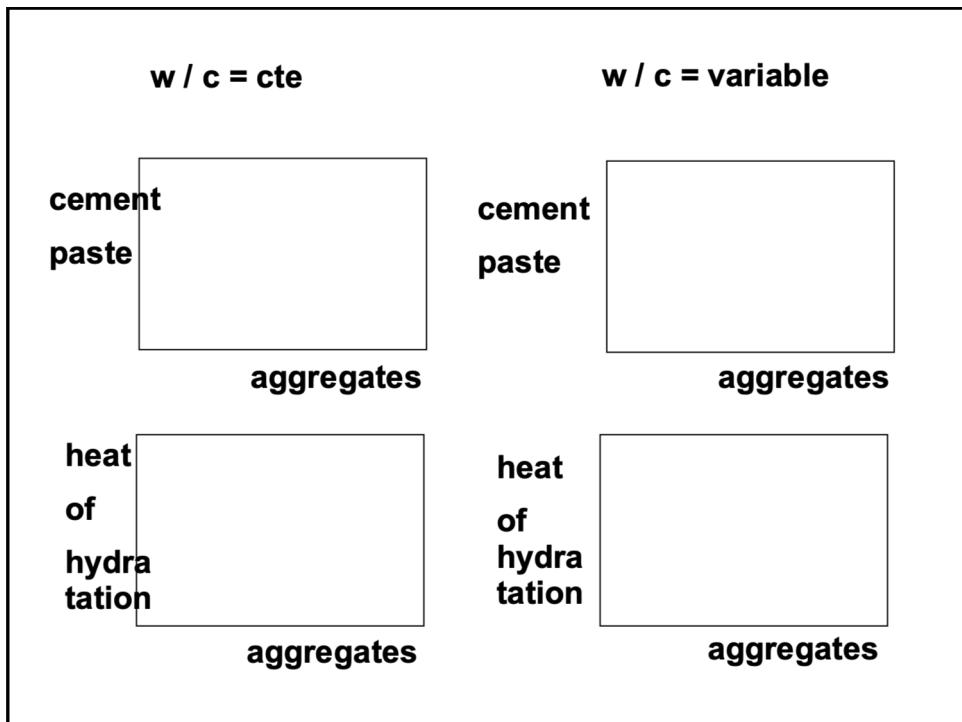


aggregates

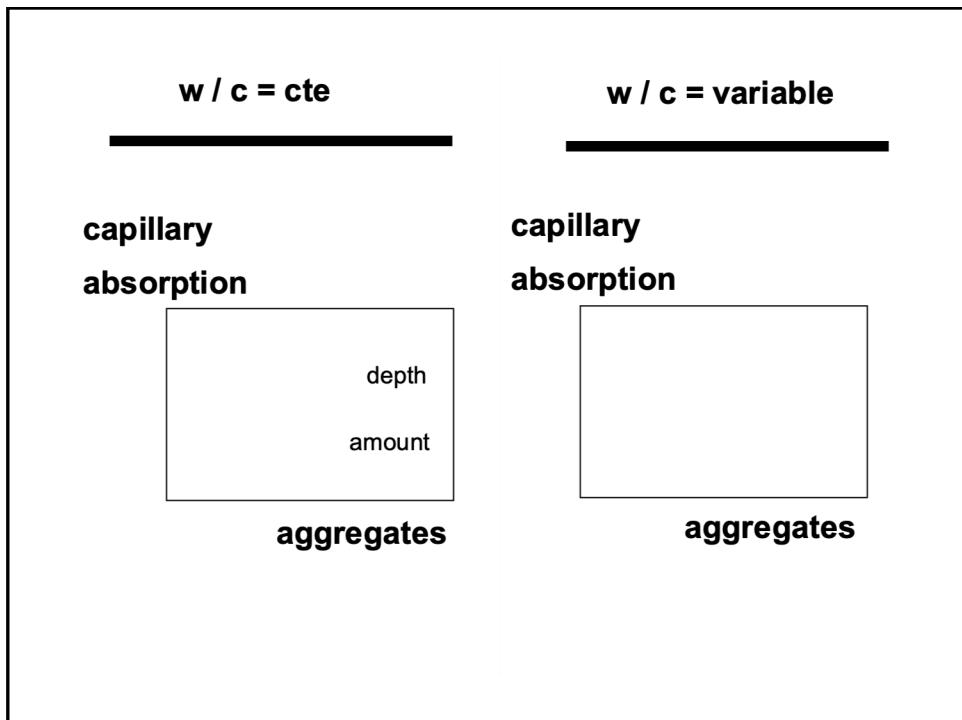
28



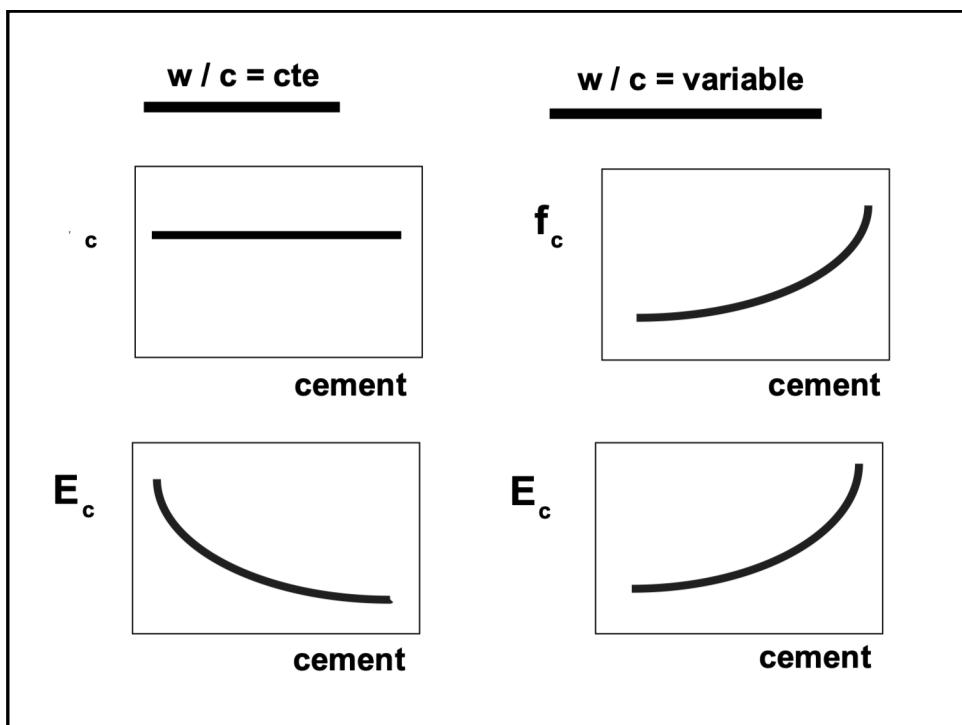
29



30



31



32

